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## Force detection, center of pressure tracking, and energy harvesting from a piezoelectric knee implant

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### Abstract

Recent developments in the field of orthopedic materials and procedures have made the total knee replacement (TKR) an option for people who suffer from knee diseases and injuries. One of the ongoing debates in this area involves the correlation of postoperative joint functionality to intraoperative alignment. Due to a lack of in vivo data from the knee joint after surgery, the establishment of a well-quantified alignment method is hindered. In order to obtain information about knee function after the operation, the design of a self-powered instrumented knee implant is proposed in this study. The design consists of a total knee replacement bearing equipped with four piezoelectric transducers distributed in the medial and lateral compartments. The piezoelectric transducers are utilized to measure the total axial force applied on the tibial bearing through the femoral component of the joint, as well as to track the movement in the center of pressure (CoP). In addition, the generated voltage from the piezoelectrics can be harvested and stored to power embedded electronics for further signal conditioning and data transmission purposes. Initially, finite element (FE) analysis is performed on the knee bearing to select the best location of the transducers with regards to sensing the total force and location of the CoP. A series of experimental tests are then performed on a fabricated prototype which aim to investigate the sensing and energy harvesting performance of the device. Piezoelectric force and center of pressure measurements are compared to actual experimental quantities for twelve different relative positions of the femoral component and bearing of the knee implant in order to evaluate the performance of the sensing system. The output voltage of the piezoelectric transducers is measured across a load resistance to determine the optimum extractable power, and then rectified and stored in a capacitor to evaluate the realistic energy harvesting ability of the system. The results show only a small level of error in sensing the force and the location of the CoP. Additionally, a maximum power of  $269.1 \mu W$  is achieved with a  $175 k\Omega$  optimal resistive load, and a 4.9 V constant voltage is stored in a 3.3 mF capacitor after 3333 loading cycles. The sensing and energy harvesting results present the promising potential of this system to be used as an integrated self-powered instrumented knee implant.

## Keywords

Total knee replacement; piezoelectric sensing; energy harvesting; orthopedic implant; biomedical sensors

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## 1. Introduction

Significant improvements in surgical technologies have made Total Knee Replacement (TKR) an option for those who suffer from pain or loss of function in the knee. Today, despite recent developments, only about 80% of patients that undergo TKR are satisfied with their surgery in terms of pain relief and function for daily activities [1]. It was shown in 1986 that several factors, such as alignment of extremities and prosthetic components, and ligament tensioning, can cause prosthetic loosening after surgery [2]. Recent studies still report loosening and instability as some of the major reasons for knee failure a few years after the operation [3]. Today, an objective and well-accepted measure of knee joint stability does not exist and better clinical assessments are needed in order to develop such a measure [4]. There are proven methods for bone alignment and knee implant component position, but ligament alignment and tensioning is still mostly performed based on the assessment of the surgeon's tactile feedback. It has been predicted that about 40% of early knee failures can be avoided using proper fixation and ligament balancing during surgery [5]. Although the importance of balance has been proven, the lack of in vivo data has limited the establishment of a correlation between intra- and postoperative loading condition, and alignment is currently not well-quantified [6].

In order to predict the functionality of the knee joint after surgery, the use of computational modeling has been suggested. However, postoperative interactions between articular geometries, passive ligamentous constraints, and muscle contribution is not well-defined. The most promoted limitations of current simulations to predict the loading condition of daily activities are oversimplified passive soft tissue representations and lack of data from joint balance after surgery [7]. In an effort to obtain postoperative data from knee replacements, an intelligent remote monitoring system was proposed by Masyib et al. [8]. The system consisted of a master and slave sensor attached with straps to the top and bottom of the knee joint to measure the relative flexion between the femur and tibia during daily activities. Using a modem and GSM network, data can be transmitted to the clinic's server to evaluate the progression and regression of the knee based on the attainable degree of flexion. The data collected with this instrumentation mostly helps physiotherapists track the external functionality of the knee but it cannot provide postoperative in vivo measurements.

D'lima et al., as one of the pioneering groups working on in-vivo knee force and moment measurement, presented an instrumented tibial tray using 4 load cells powered by an external coil around the patient's knee [9]. The device presented by Heinlein et al. [10] was the first attempt to develop an in-vivo system capable of six force and moment component measurements. The device consisted of 6 strain gauges and a telemetry system located in the stem of a two-piece tibial component with an external coil as the power source, resulting in an overall thickness increase of the tibial tray of 5 mm. The results of tibiofemoral force

measurement obtained postoperatively from implanted devices designed by both D'lima and Heinlein present a good fit with modeling simulation results for normal function of the knee [9, 10]. In another study, Crescici et al. [11] presented a new design for an instrumented polyethylene bearing with 3 magnetoresistive sensors and an embedded wireless data transmission circuit. This system was inductively powered by an external coil and was evaluated under sinusoidal input force to verify the measurement system. The obtained results showed variability in measured data which was speculated to be a result of nonlinear material behavior and hysteresis effects. The main limitation with the abovementioned knee sensory systems is the external power source requirement of the devices. This can limit the application of the system to laboratories and obviate the device to perform continuously at the patient's convenience.

Piezoelectric transducers present the potential to be implemented in various sensing and energy harvesting applications [12, 13]. Several wearable and implantable piezoelectric energy harvesters have been introduced in the literature in order to provide the required energy for low-power electronics by harvesting energy from human motion [14, 15]. In 2005, Platt et al. [16] showed that it is feasible to utilize piezoelectric transducers in TKR as sensors and energy harvesters. More recently, Almouahed et al. [17, 18] suggested utilizing piezoelectric ceramics in the tibial component of a total knee replacement to measure the total axial force applied to the bearing and to track the location of the center of pressure (CoP). Center of pressure is defined as the point of application of the sum of the medial and lateral forces (i.e. the forces acting in the medial and lateral compartments) acting between the femoral component and the ultra-high molecular weight (UHMW) polyethylene bearing of the knee joint. For reference, a schematic of a TKR is illustrated in Figure 1(a). Although the proposed system can provide self-powered in vivo measurement during normal function of the joint, the original implant design is modified to implement the sensory system. The change in the overall dimension and design of the knee implant requires manufacturers and surgeons to modify their design and surgical techniques, which have been obtained as a result of several years of experience.

In order to tackle the power source and implant design modification limitations of existing approaches, a novel design of a TKR bearing with embedded piezoelectric transducers is proposed in this study. Implanted piezoelectric transducers in the UHMW bearing of the TKR can provide self-powered sensing ability directly from the bearing as a result of the applied force through the femoral component [19]. Furthermore, by encapsulating the piezoelectric transducers inside the existing knee bearing, the original design of the implant can be preserved. The conceptual design explored in this study aims to provide the ability of sensing knee loads and transmitting data once per day with the help of the power harvested from daily activities. In addition, the application of embedded piezoelectrics can be extended to structural health monitoring (SHM) on the bearing to monitor for loosening, wear, and fracture in the implant (which will be the focus of our future work). The design consists of two lead zirconate titanium (PZT) transducers located in each of the medial and lateral compartments of the UHMW insert (total of four PZTs). First, the arrangement of piezoelectric transducers inside the bearing is varied and the best arrangement is selected using finite element (FE) simulation. Next, the ability of the employed PZT elements to detect the total applied force on the bearing and track the movement of the center of pressure

is experimentally investigated through a series of twelve tests that vary the relative position of the femoral component and UHMW bearing. Finally, the energy harvesting capability of the design in harvesting power from normal knee function is studied. A series of resistor sweep tests are first performed to obtain the maximum theoretical harvestable power from the device. The practical attainable power is then measured using a bridge rectifier and capacitor circuit.

## 2. Design

Measuring the quantity of total force and tracking the location of the center of pressure on the knee bearing surface are the intended sensing functions for the instrumented TKR in this study. Four piezoelectric transducers, located on the bottom surface of the UHMW bearing, are employed to measure the force and location quantities. Figure 1(b) shows this instrumented TKR bearing design with the incorporated piezoelectrics; two piezoelectrics are placed in each compartment of the bearing (medial and lateral) to ensure measurement of each compartmental force, thus allowing calculation of the total applied force and the CoP. In addition to sensing, the piezoelectric transducers are able to harvest energy from the compression load acting on the bearing during walking. The intended functionality of this system is to measure the desired quantities and transmit to an external computer once a day, thus, the amount of energy harvested and stored during the day should be sufficient to power the sensory system during the sensing operation (which is likely to take less than one minute).

Due to the importance of axial alignment of the knee joint [2], the compressive axial force between the femoral and tibial components of the TKR is considered as the main force component acting on the joint. As a result of the applied force on the bearing, reaction forces are created on each piezoelectric transducer. By measuring these individual force quantities, the amount of total axial force on the UHMW component as well as the location of the CoP can be calculated. Recall, CoP is the average location of contact areas on the bearing in which the total force is acting. In other words, CoP is the point where the moment of the total force applied to the bearing is zero. Tracking the movement of the CoP provides valuable information about medial-lateral and anterior-posterior alignment of the joint, as well as the contact mechanism of the femoral component and tibial bearing [21]. The location of the CoP for a bearing with two contact points (CPs) located on the medial and lateral compartments of the bearing is shown later in Figure 4(a).

## 3. Finite Element Simulation

### 3.1. Simulation Setup

Based on the conceptual design shown in Figure 1(b), a FE study is performed in this section on a knee implant consisting of a femoral component and an instrumented knee bearing with four embedded piezoelectric transducers. The aim of the FE analysis is to investigate the effect of the different locations of piezoelectrics (i.e. arrangement of the sensors) inside the bearing on the sensing performance of the device. Therefore, several patterns of piezoelectric locations are chosen for the system and the ability of the piezoelectric elements to measure the total force applied to the bearing and the location of the CoP is studied. The

FE analysis is conducted using ANSYS software and the FE model is shown in Figure 2(a). The model consists of SOLID187 elements (3-D 10-node tetrahedral solid element with three translational degrees of freedom) for the femoral component and bearing, SOLID227 elements (3-D 10-node coupled-field tetrahedral solid element with five translational, thermal, and electrical degrees of freedom) for the piezoelectric elements, and CONTA174 and TARGE170 (surface elements with the same geometric characteristics as the solid elements) for contact surfaces, and contains 384,231 nodes and 256,392 elements. The element size for PZTs, and bearing and femoral component are 0.6 mm and 1.2 mm, respectively, with a maximum aspect ratio of 8. The mesh is finely refined on the contact surfaces and on the corners, and a mesh refinement study is initially conducted to ensure that the simulation results converged. Frictional boundary conditions are applied between the femoral component and bearing as well as between the PZTs and bearing with a friction coefficient of 0.12 [22].

The CAD geometry of the femoral and tibial components is obtained by 3D scanning a real knee implant, and the bearing is modified in order to accommodate four piezoelectric transducers. Four 8 mm diameter and 2 mm depth pockets are removed from the bottom surface of the bearing. Piezoelectric disc transducers with a diameter of 8 mm and thickness of 2.5 mm are used. The pockets are designed to be shallower than the piezoelectric transducers in order to ensure full load transmissibility to the PZTs during the tests and, therefore, maximum sensing capability of the system [19]. The material for the bearing is chosen to be PLA (polylactic acid) in order to match the material used in the experiment (see Sec. 4.1). The piezoelectric transducers are 25-layer NCE51 (PZT-5A) PZT stacks (Noliac, Inc.). The material properties of PLA and the piezoelectric transducers are listed in Table 1. The piezoelectric transducers are polarized in the y-direction.

Two angular parameters, as shown in Figure 2(b), are defined in order to control the location of the piezoelectric transducers. The locations of PZT1 and PZT2 are specified with angular parameters  $\alpha_1$  and  $\alpha_2$ , respectively. The  $\alpha_1$  parameter is allowed to take on values of 50°, 90°, and 130°, and the  $\alpha_2$  parameter is allowed to take on values of 50°, 70°, 90°, and 130° in order to investigate twelve different patterns. Note, PZT3 and PZT4 are located in a symmetric arrangement to PZT1 and PZT2, respectively. A realistic knee loading profile obtained from OpenSim (an open source biomechanical simulation software) is utilized as the axial input load (y-direction in Figure 2(a)) of the system [19]. The force profile is shown in Figure 3. The knee bearing and femoral component are initially center-aligned based on the geometric centers of the components, and constrained in the x- and z-directions for all simulations. The bottom face of the piezoelectric transducers is restrained in all directions. The effective force applied to each PZT and the pressure distribution on the contact surface of the bearing and femoral component are collected from the transient FE simulation with an initial timestep of 0.01 sec and 120 steps. The true locations of the contact areas are obtained from the pressure distribution result on the top surface of the bearing, and the true location of the CoP is calculated from the average location of the contact points. The location of the CoP as measured by the four piezoelectric transducers can be calculated using the equilibrium of moments as follows:

$$x_{CoP} = \frac{\sum_{i=1}^4 x_i F_i}{F_T}, \quad (1)$$

$$z_{CoP} = \frac{\sum_{i=1}^4 z_i F_i}{F_T}, \quad (2)$$

where  $x_{CoP}$  and  $z_{CoP}$  are the Cartesian coordinates of the CoP,  $x_i$  and  $z_i$  are the coordinates of  $i$ th piezoelectric transducer,  $F_i$  is the reaction force on  $i$ th transducer, and  $F_T$  is the total force applied on the bearing, which is the summation of the individual forces, as given by

$$F_T = \sum_{i=1}^4 F_i. \quad (3)$$

On the other hand, the true location of the CoP can be calculated as the average location of the nodal pressures obtained for all of the nodes located on the top surface of the bearing as follows:

$$x_{CoP}^n = \frac{\sum_{i=1}^{N_t} x_i^n P_i^n}{P_T}, \quad (4)$$

$$z_{CoP}^n = \frac{\sum_{i=1}^{N_t} z_i^n P_i^n}{P_T}, \quad (5)$$

where  $x_{CoP}^n$  and  $z_{CoP}^n$  are the true location of the CoP obtained from nodal pressure quantities,  $x_i^n$  and  $z_i^n$  are the coordinates of  $i$ th node,  $P_i^n$  is the nodal pressure of  $i$ th node,  $N_t$  is the total number of nodes located on the top surface of the bearing, and  $P_T$  is the total pressure on the top surface.

### 3.2. Simulation Results

Results of the FE simulations performed for different angles of  $\alpha_1$  and  $\alpha_2$  are summarized in Table 2. Twelve simulations are accomplished and the error in the total force and deviation

in the location of the CoP are calculated using Eqs. (1)–(5). It can be seen from the results that the error in measured total force quantities is zero for all simulations, which indicates convergence of the FE model. On the other hand, the deviation in the location of the CoP varies with the change in the angular parameters. Based on the results, the arrangement used in Simulation 1 with  $\alpha_1=130^\circ$  and  $\alpha_2=90^\circ$  demonstrates the minimum deviation in the measured location of the CoP obtained from the PZTs from the true location obtained from the pressure distribution on the top surface of the bearing. Figure 4(a) represents the pressure distribution on the bearing obtained from Simulation 1. For more clarity, the locations of the two CPs on the compartments of the bearing and of the CoP are shown in this figure as well. Figure 4(b) shows the exact location of the piezoelectric transducers for this chosen arrangement (Simulation 1). The maximum total deviation of the location of the CoP for this arrangement is only 0.32 mm. The chosen arrangement is utilized in the next section to fabricate a prototype of the device in order to experimentally investigate the sensing and energy harvesting performance of the suggested system.

## 4. Experiment

### 4.1. Fabrication

A prototype of the instrumented TKR bearing is fabricated via 3D printing based on the design chosen from the FE simulation, shown in Figure 4(b). 3D printing offers the ability to quickly and easily develop and test prototypes of various designs, therefore, it is selected as the fabrication method used in this work. Printable UHMW filament is not currently available on the market, therefore, PLA is chosen. Although the material properties of PLA are not identical to UHMW, the two materials exhibit similar mechanical behavior under compressive loading, therefore, PLA is deemed a suitable material for use in this study [25]. Similar to the design used in the FE simulation, four pockets are placed on the bottom surface of the bearing symmetrically to accommodate the piezoelectric transducers. Pockets shallower than the PZTs guarantee full force transmissibility to the transducers and maximum sensing and energy harvesting performance. As described in Sec. 3.1, the piezoelectric transducers are 25-layer NCE51 (PZT-5A) PZT stacks. Stack geometries can provide relatively high coupling properties which are optimal for sensing applications. Additionally, the matched impedance of piezoelectric stacks for optimum energy harvesting is on the order of hundreds of  $k\Omega$  (as opposed to  $M\Omega$  for similar monolithic transducers), which is appropriate for realistic energy harvesting circuitry [26].

The material properties of the piezoelectric stacks and PLA material have been previously listed in Table 1. The manufactured knee bearing with incorporated PZTs is shown in Figure 5. It can be seen that an arrangement of grooves is incorporated on the bottom face of the bearing for routing of the wires soldered to the piezoelectric electrodes and connected to the data acquisition circuitry. It is necessary to note that in the eventual design of the instrumented implant, the external leads will be removed and a set of embedded electronics will be incorporated to perform data acquisition, processing, and transmission, as well as power storing.



## 4.2. Test Setup

In order to investigate the performance of the integrated bearing and piezoelectric system, a series of tests is performed on the fabricated prototype. The aim of the experimental tests is to evaluate the ability of the fabricated system to measure the total axial applied force and the location of the CoP on the bearing, as well as harvest energy during the loading cycle. Figure 6(a) shows the overall experimental setup used to test the prototype instrumented knee bearing, which allows the load to be applied to the bearing through the femoral component of the TKR. A closer view of the test setup detailing the femoral fixture, the femoral component, the knee bearing with embedded PZT transducers, and the bearing fixture is shown in Figure 6(b). Initially, the relative position of the femoral component and bearing is set to an arbitrary zero position in which the femoral component and the bearing are visually center-aligned in both medial-lateral and anterior-posterior directions.

The realistic knee loading profile described in Sec. 3.1 is utilized as the axial input load of the load frame. The generated voltage from the piezoelectrics is collected via two distinct sets of circuits; one circuit for sensing and two types of circuits for energy harvesting, and measured using an NI 9215 data acquisition module and a LabVIEW program (National Instrument Corp.). The sensing circuit is designed to measure the output voltage of each piezoelectric individually in order to sense the quantity of applied force on each transducer. The energy harvesting circuits, on the other hand, are designed to extract the maximum power from all the piezoelectric generators across a load resistance, and to rectify and store the total generated power from all the piezoelectrics in a single storage device. In practice, in a real instrumented knee implant, the energy stored via the energy harvesting circuit would be used to power an embedded sensory circuit that collects, processes, and transmits the data.

**4.2.1. Sensing Tests—**In order to measure the force and location of the CoP, the individual voltage signals from each piezoelectric transducer must be obtained and processed. To do so, a load resistance of 100 k $\Omega$  is placed in parallel with each piezoelectric element and the voltage signal is measured across the resistor. The circuit diagram utilized for data collection from each piezoelectric transducer is presented in Figure 7. The voltage signals are processed with the help of a MATLAB code to obtain the measured force and location of the CoP. The actual location of the CoP on the bearing surface is obtained from an image processing code for the recorded contact areas using a medium-range Prescale pressure sensitive film (Fujifilm Corp.) placed on the interface of the tibial component and the bearing. Twelve tests are performed on the fabricated bearing to investigate the ability of the sensory system to measure the force and track the location of the CoP for different contact locations. For the first six tests (Test 1–6), the translational location of the femoral component on the bearing is varied in the medial-lateral direction, and for the second six tests (Test 7–12), the location is varied in the anterior-posterior direction using the bearing fixture shown in Figure 6(b). The movement directions are shown in Figure 1(a). Different translational locations are achieved by moving the bearing along the medial-lateral (x) and anterior-posterior (z) axes in 1.5 mm increments. For Test 1 and Test 7, the bearing and femoral component are visually center-aligned, and the relative locations for the remainder of the tests are varied with reference to these two initial locations. The relative location of



the femoral component and the bearing for all the sensing tests is listed in Table 3. Note, due to the curved interface of the femoral component and bearing, it is expected that the increments in CoP movement will not be equal to the 1.5 mm increments of the knee bearing movement. In order to calculate the force from the collected voltage signals, the first order governing equation of a piezoelectric stack connected to a load resistance under low-frequency uniaxial compression loading is employed [27]:

$$C_p^{eff} \frac{dV(t)}{dt} + \frac{V(t)}{R} = d_{33}^{eff} \frac{dF(t)}{dt}, \quad (6)$$

where  $V(t)$  is the generated voltage,  $F(t)$  is the applied force on the PZT,  $R$  is the resistive load connected to the PZT,  $d_{33}^{eff}$  is the effective piezoelectric strain coefficient, given by

$$d_{33}^{eff} = Nd_{33}, \quad (7)$$

where  $N$  is the number of piezoelectric layers, and  $d_{33}$  is the piezoelectric strain coefficient.  $C_p^{eff}$  is the effective capacitance of the PZT stack, given as

$$C_p^{eff} = \frac{N\epsilon_{33}^T A}{h}, \quad (8)$$

where  $\epsilon_{33}^T$  is the dielectric permittivity,  $A$  is the cross-sectional area of the stack, and  $h$  is the thickness of each layer. It should be noted that the highest excitation frequency found in the OpenSim knee load profile is several orders of magnitude less than the fundamental thickness resonance frequency of the stack, thereby warranting the use of a non-resonant first-order model. The force quantities measured on each piezoelectric transducer can be used to calculate the total applied force by simple summation of the four reaction forces, as presented in Eq. (3). The location of the CoP can then be calculated using the moment equilibrium equations expressed in Eqs. (1) and (2).

**4.2.2. Energy Harvesting Tests**—The instrumented bearing proposed in this work consists of four piezoelectric transducers, therefore, various wiring configurations of the PZTs are possible. The electrical configuration of the PZTs (series vs. parallel vs. combination of series and parallel) affects the generated voltage and optimal resistive load for maximum generated power. In piezoelectric energy harvesting systems, the amount of harvestable power depends on the relative impedance of the load and the piezoelectric generators, with optimal extracted power occurring when the impedance is matched [28]. In order to determine the ideal electrical configuration, three unique wiring configurations are first investigated in this section to determine the most appropriate configuration suitable to power a low-power wireless biomedical sensing circuit from the literature in terms of generated voltage level and optimal resistive load. Once the ideal configuration is selected, the optimum extractable power (theoretical power) from the piezoelectric system is

determined through a series of resistor sweep tests. Following this analysis of the maximum theoretical harvestable power, a second set of experiments is conducted to determine the practical harvestable power (practical power) through a bridge rectifier and smoothing/storage capacitor energy harvesting circuit.

First, three combinations of piezoelectric wiring connections are considered, and the behavior of each case is investigated analytically and numerically to determine the best configuration. It is necessary to note that the analytical solution is conducted for an arbitrary harmonic loading condition to obtain a parametric understanding of the ratios of optimum resistor, optimum power, and peak voltage for each configuration to those of a single PZT system and for the sake of comparison. Afterward, quantitative results are also developed for the actual OpenSim load profile using a numerical solution. Figure 8 shows the three arrangements considered, whereby the PZT transducers are placed in series, parallel, and a combination of series and parallel (Figure 8(a), (b), and (c), respectively).

For a single piezoelectric transducer under a dynamic load of  $F(t)$  and connected in parallel to a resistor  $R$ , the governing electromechanical equation is presented in Eq. (6). For harmonic excitation, the peak voltage can be obtained from Eq. (6) as

$$V = \frac{j\omega d_{33}F}{\frac{1}{R} + j\omega C_p}, \quad (9)$$

where  $\omega$  is the frequency of excitation and  $j$  is the imaginary unit. Then, the peak power can be written as  $P = \frac{V^2}{R}$ , and the optimum resistive load to obtain the maximum power can be calculated from  $\frac{dP}{dR} = 0$ . As a result, the optimum resistive load ( $R_{opt}$ ) is

$$R_{opt} = \frac{1}{j\omega C_p}. \quad (10)$$

Based on Eqs. (6), (9), and (10), the governing equation, optimum resistor, maximum power, and peak voltage with the optimum resistor for all three energy harvesting circuits shown in Figure 8 are developed and listed in Table 4 in comparison with a single PZT connected to a resistive load. Although the force profile used in this study (OpenSim profile) is not harmonic, due to the periodic behavior and consistent frequency content of the profile, the relative ratios of optimum resistor, maximum power, and peak voltage provided in Table 4 (presented in “Harmonic” columns) are valid for the sake of comparison. On the other hand, substituting the OpenSim force profile and the material properties of PZT stacks, as listed in Table 1, into Eq. (6), the optimum resistor, maximum power, and peak generated voltage quantities are also numerically calculated and added to Table 4 for each configuration (presented in “OpenSim” columns).

A published study on the development of a low-power wireless circuit designed for knee implants shows a 1.2 V to 3.6 V voltage requirement and an equivalent circuit resistance of

about 31  $k\Omega$  [29]. Based on the requirements of the aforementioned circuit, the configuration with all four PZTs connected in parallel to a resistive load is chosen as the ideal arrangement for the energy harvesting tests in this work.

In order to determine the optimum extractable power (theoretical power) from the piezoelectrics, the load resistor is swept from 10  $k\Omega$  to 1  $M\Omega$  and the voltage across the resistor is measured. Again, the voltage signals are imported into a MATLAB program in order to process and calculate the average generated power by the piezoelectrics. The average power is calculated as

$$P_{avg} = \frac{v_{rms}^2}{R}, \quad (11)$$

where,  $v_{rms}$  is the RMS voltage given by

$$v_{rms} = \sqrt{\frac{1}{T} \int_0^T v^2(t) dt}, \quad (12)$$

in which,  $T$  is the time period of voltage signal.

While the theoretical power can be obtained using this technique, the practical harvestable power from the piezoelectric system will be less than the theoretical value due to losses in the circuitry required to condition the harvested energy for use. In real-world applications, the generated voltage from the piezoelectric transducers under cyclic loading is in the form of a time varying signal with a high level of fluctuation, therefore, it needs to be rectified and stored prior to use. Thus, in addition to the theoretical power circuitry introduced for the resistor sweep tests, a practical energy harvesting circuit consisting of a basic bridge rectifier and smoothing/storage capacitor is also used in this work. The circuit diagram for this energy harvesting circuit is illustrated in Figure 9, where the four piezoelectrics are connected in parallel to the bridge rectifier (since the mechanical loading on each transducer is in phase, voltage cancellation is not of concern). The stored energy in the capacitor is measured using the NI DAQ in terms of the capacitor voltage.

### 4.3. Test Results

**4.3.1. Sensing Test Results**—Figure 10(a) presents the total force profile measured from the piezoelectric transducers along with the actual applied force to the knee bearing measured by the built-in load cell of the load frame for Test 1 (recall, twelve tests are conducted, as described previously in Table 3). Note, a 20-point moving average filter has been applied to the voltage signals to help eliminate measurement noise. Comparing the two diagrams, it can be seen that the measured force profile matches with the applied force profile for higher quantities of force. On the other hand, deviations of the measured force from the actual profile at the beginning and end of the test (where lower force amplitudes occur) are noticeable. The error in these areas can be partially attributed to low signal-to-

noise ratio in the collected data in these regions and the corresponding inaccuracies caused by filtering the data. Moreover, preliminary tests on the piezoelectric stacks show nonlinear behavior in the  $d_{33}$  coefficient, while a constant coefficient is used for data processing in this study. This error can be reduced or potentially eliminated by testing in a low-noise environment, using more precise data acquisition equipment and signal processing techniques, and applying a variable piezoelectric strain coefficient in the calculation. Similarly, the force profile is obtained for all of the other tests and the error in measured peak forces is plotted in Figure 10(b) for all twelve tests. Overall, the error in force sensing is less than 2.5% of the total force applied to the bearing for all twelve tests.

In addition to force amplitudes, the location of the CoP is analyzed. Figure 11 shows the measured locations of CPs and CoP from the pressure sensitive films for Test 1. The measured CoP locations for the six tests with the bearing moved in the x-direction and the six tests with the bearing moved in the z-direction are compared to the true CoP locations recorded by the pressure films and plotted in Figure 12(a) and (b), respectively. Comparing the measured location of the CoP from the piezoelectric sensors with the actual coordinates obtained from the pressure sensitive films, the deviation in calculated CoP location from the actual location can be obtained. Note, while the knee bearing is moved along the x- and z-axis with 1.5 mm increments, movement of the true location of the CoP represents uneven increments due to the complex contact surfaces of the femoral component and the bearing. From the two plots, it can be observed that the piezoelectric sensors are able to track the movement in the location of the CoP for a wide range of bearing and femoral component relative movement with a small deviation of less than 0.5 mm.

**4.3.2. Energy Harvesting Test Results**—First, the resistor sweep test is performed on the piezoelectric system. The average power harvested from the piezoelectrics is plotted in Figure 13(a) along with the average power calculated analytically using Eqs. (6) and (11). The diagram shows that the simulation and experimental results are in good agreement. A maximum extracted power of  $269.1 \mu W$  is achieved with a  $175 k\Omega$  optimal resistive load experimentally, whereas, the simulation shows a maximum average power of  $268.4 \mu W$  for an optimum resistive load of  $150 k\Omega$  (as previously presented in Table 4).

Next, in order to determine a better understanding of the amount of practical harvestable energy, the total voltage signal obtained from the piezoelectrics using the bridge rectifier and smoothing/storage capacitor is obtained. The test is run for 4,000 s, which is equivalent to 3,333 gait cycles. It is necessary to note that an average of about 10,000 steps (cycles) per day is reported for a healthy person [30, 31]. However, considering the reduced level of activity in patients after knee surgery, a reduced number of steps (gait cycles) per day is expected during the recovery period, therefore, 3,333 gait cycles can be considered a reasonable representation of the total daily number of steps for a patient after undergoing a knee replacement procedure. Figure 13(b) shows the capacitor voltage diagram versus time. Although the piezoelectric transducers were continuously charging the capacitor, it can be seen that the voltage reaches the steady state quantity of 4.9 V after about 3000 s. The constant voltage of the capacitor represents the maximum voltage generated from the piezoelectric transducers after the bridge rectifier (which includes losses in the diodes) and accounts for self-discharge in the capacitor as well as loading from the data acquisition

system. It should be noted that the amount of voltage loss in the circuit can be decreased using more ideal components such as low-loss diode bridges and thin film batteries or supercapacitors. The total energy stored in the capacitor after 3000 cycles is calculated from Figure 13(b) as 40 mJ (13.3  $\mu$ W average power). It has been reported that an embedded low-power data processing and transmission system designed for orthopedic implants consumes 45  $\mu$ W and 3.2 mW in data collecting and transmission modes, respectively [29]. As a result, the amount of power stored in the capacitor is sufficient for 9 min of sensing and data processing, and 5 sec of data transmitting. Considering the target function of the instrumented implant developed in this work (harvesting throughout the day and sensing/ data transmitting once per day), these results show promising potential of embedded PZTs to supply power to a low power force measuring and telemetry system for knee implants. Note, the power rectified and stored in the capacitor is about 20 times less than the maximum power obtained from the piezoelectric harvesters using the resistor sweep tests (theoretical power). Therefore, using more advanced electronics with impedance matching capability, the energy harvesting efficiency of the system can be improved and the duty cycle of sensing and energy harvesting system can be reduced.

## 5. Conclusion

A novel design of an instrumented knee implant with four embedded piezoelectric transducers for sensing force magnitude and tracking center of pressure (CoP), as well as energy harvesting for self-powered operation is proposed in this study. A duty cycle operation is considered for the device whereby energy is harvested from daily activities and then used at the end of the day to power the sensing and data transmission electronics. First, the best arrangement of piezoelectric transducers is selected via finite element (FE) analysis with regard to the sensing performance of the device in detecting force magnitude and CoP location. Next, a 3D printed prototype of the device with the chosen sensor configuration is fabricated and employed in a series of experimental tests. Using a load frame, a realistic knee compression load profile is applied on the instrumented bearing via the femoral component of an actual knee implant. Sensing and energy harvesting tests are conducted individually with different electrical circuits. The sensing ability of the device is studied by processing the individual generated voltage signals from the piezoelectric transducers measured across simple load resistors. The total applied force and the location of the CoP are measured by the piezoelectrics and compared to the true quantities obtained from the load frame and pressure sensitive films placed on the top surface of the bearing. Two circuits are considered for the energy harvesting tests, both of which place all four PZTs in parallel. First, the optimum theoretical harvestable power is determined by a resistor sweep circuit where a simple load resistor is placed across the piezoelectrics. Next, a voltage rectifier and storage capacitor circuit is employed to obtain the practical harvestable power from the PZTs. The sensing results showed an error of less than 2.5% in force sensing and a deviation of less than 0.5 mm in tracking the location of the CoP when the relative positions of the femoral component and bearing are varied. The resistor sweep tests showed that with an optimum load, an average power of up to 269.1  $\mu$ W (theoretical power) can be harvested from the piezoelectric transducers. In addition, the average rectified and stored power (practical power) was found to be 13.3  $\mu$ W and was shown to be sufficient to power a

biomedical sensing and data transmission circuit from the literature with a low duty cycle. The promising sensing and energy harvesting results obtained in this study show the potential of the instrumented knee implant to be employed as a self-powered knee sensory system.

## Acknowledgments

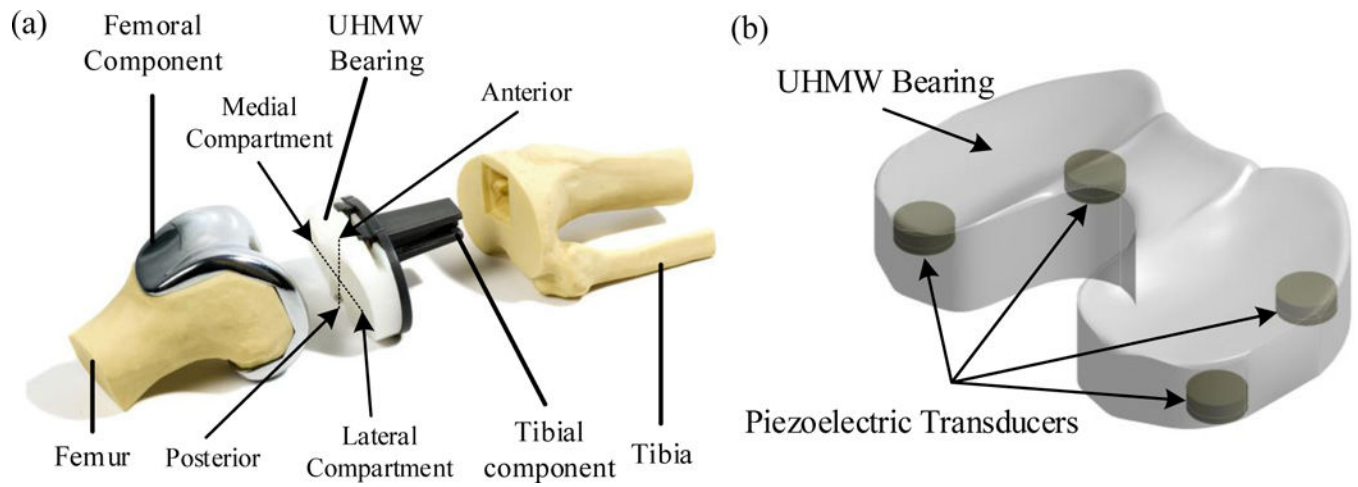
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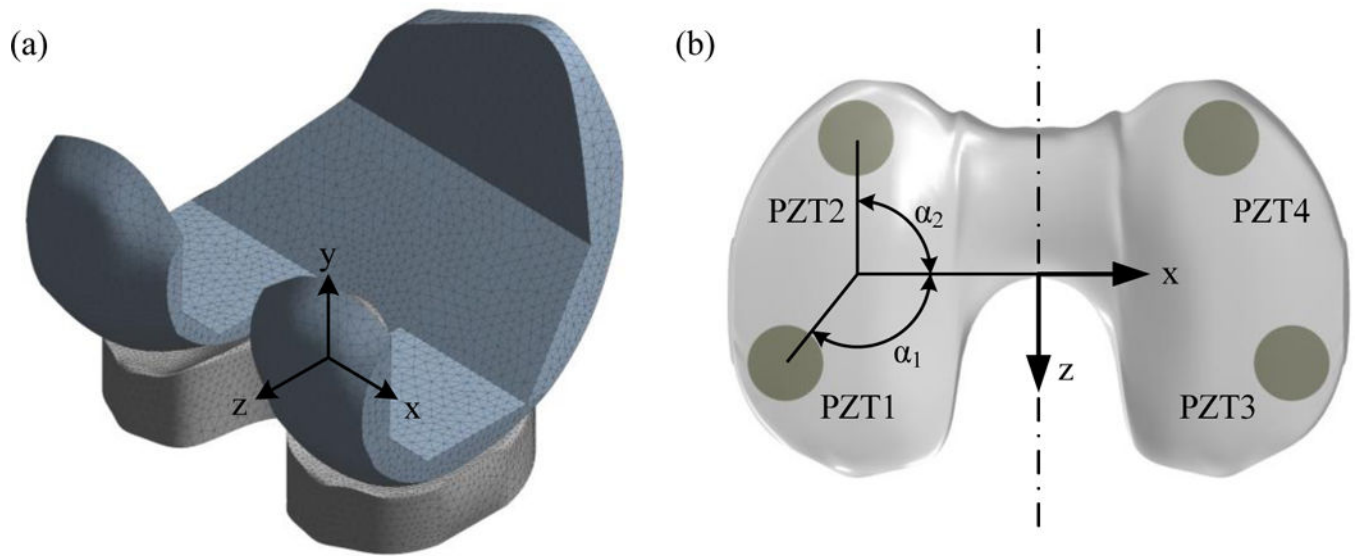
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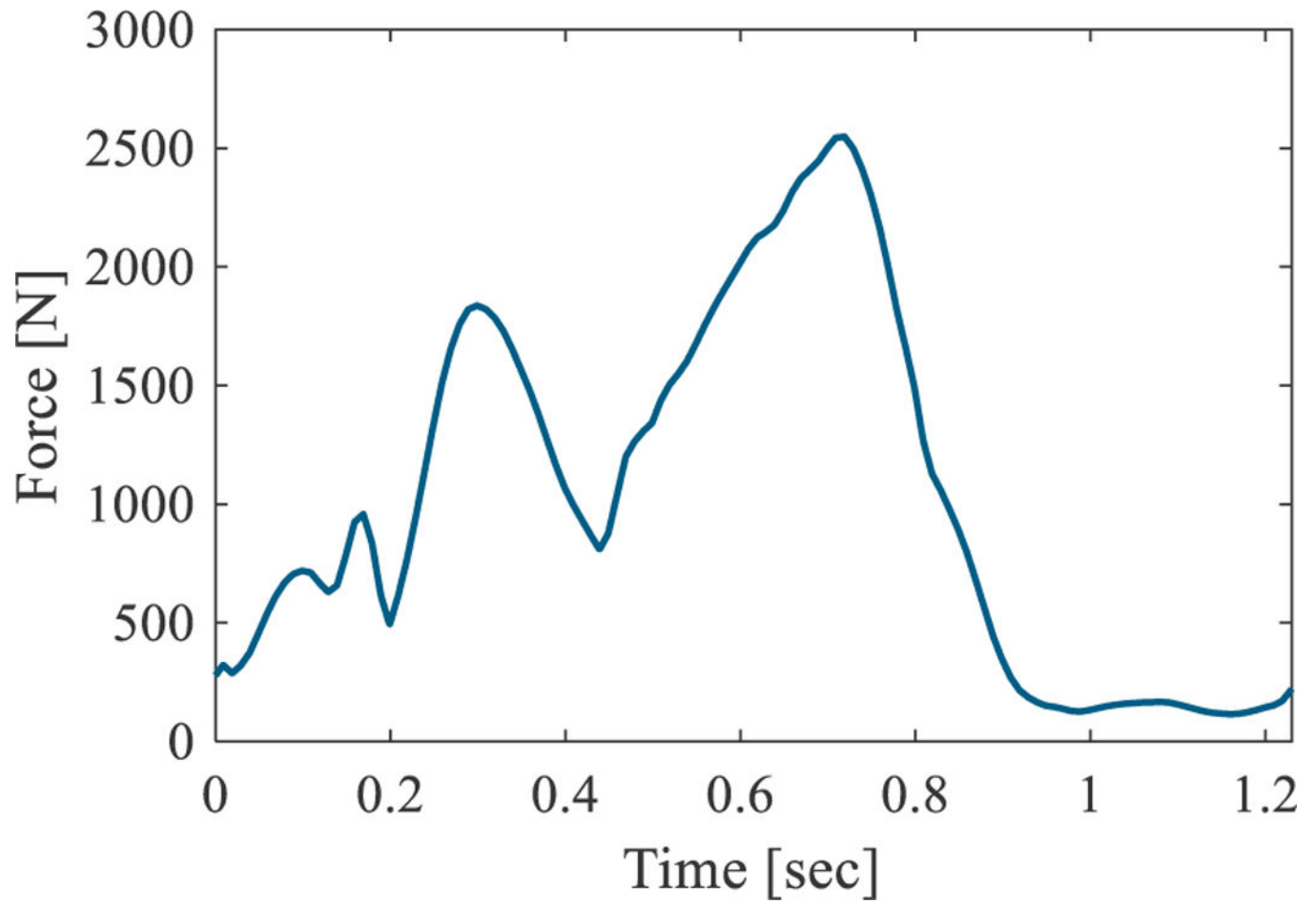




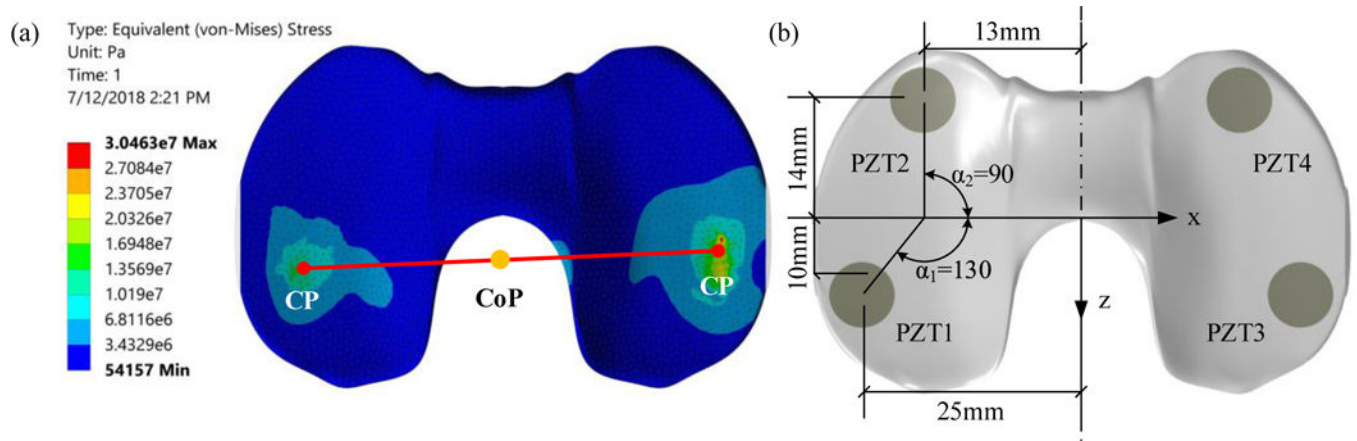
**Figure 1.** Schematic of (a) total knee replacement (right knee) [20], and (b) UHMW bearing with four embedded piezoelectric transducers.



**Figure 2.**  
 (a) FE model of femoral component and instrumented bearing, and (b) angular parameters defined for FE analysis.

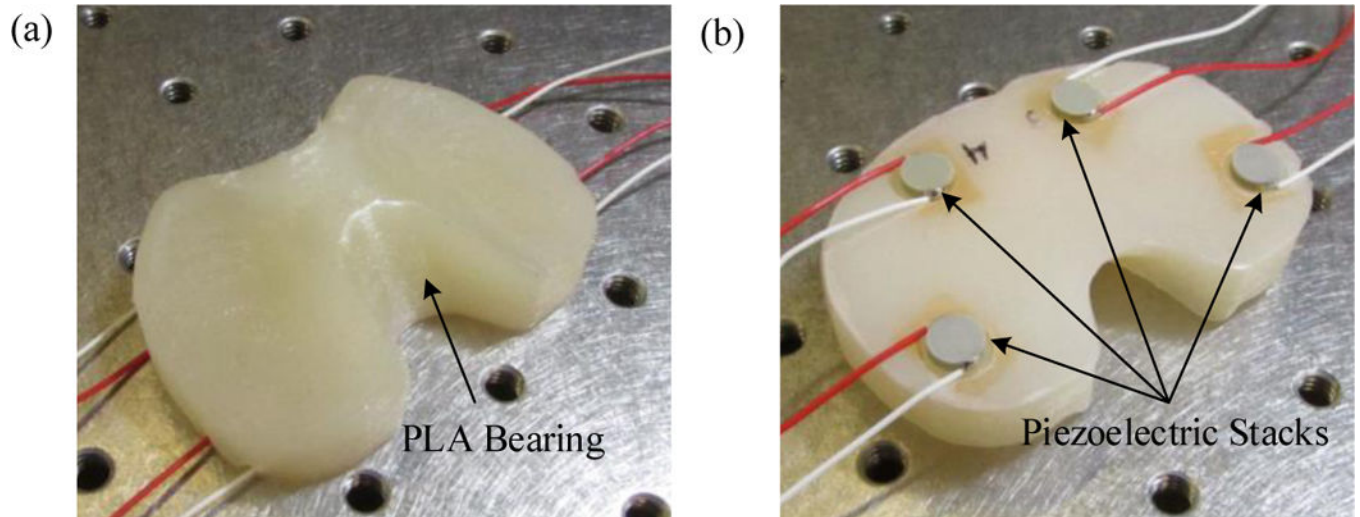


**Figure 3.**  
Realistic knee load profile obtained from OpenSim.

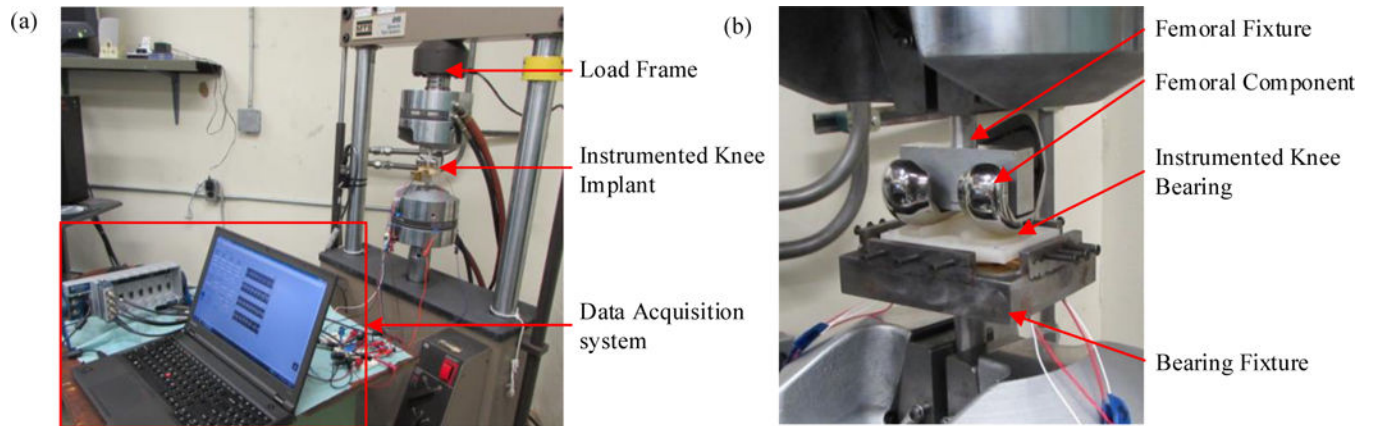


**Figure 4.**

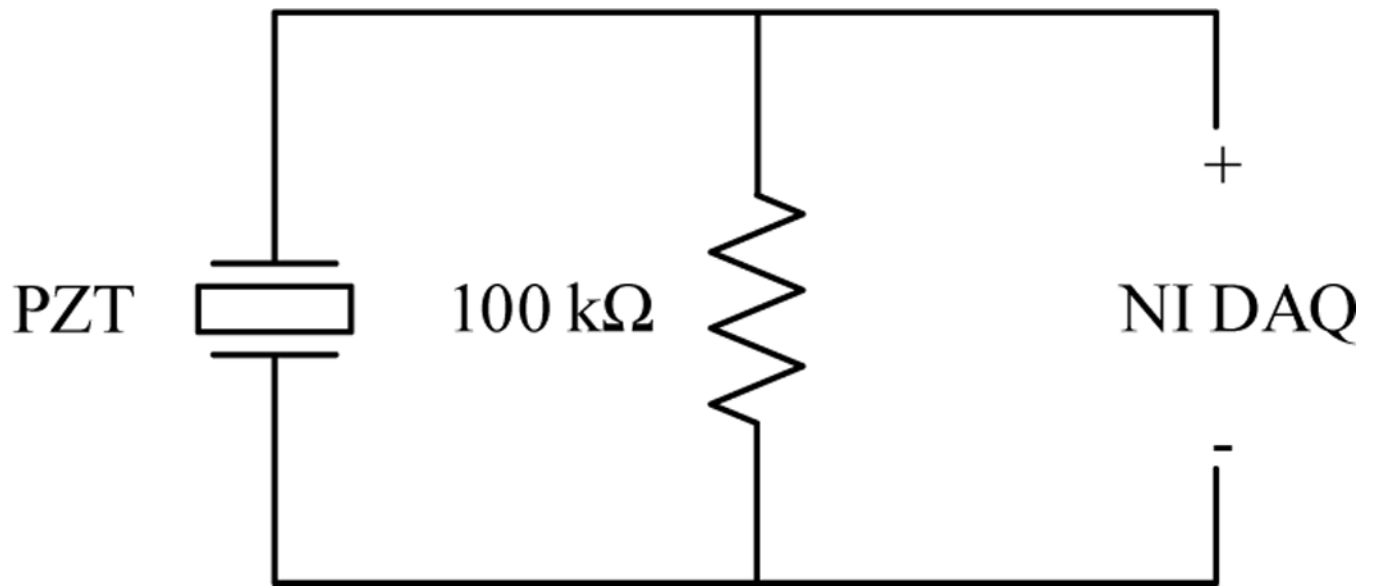
(a) Pressure distribution on the bearing obtained from FE analysis, and (b) chosen arrangement of PZT sensors (top view).



**Figure 5.** Fabricated instrumented knee bearing equipped with four piezoelectric stacks (a) top view, and (b) bottom view.

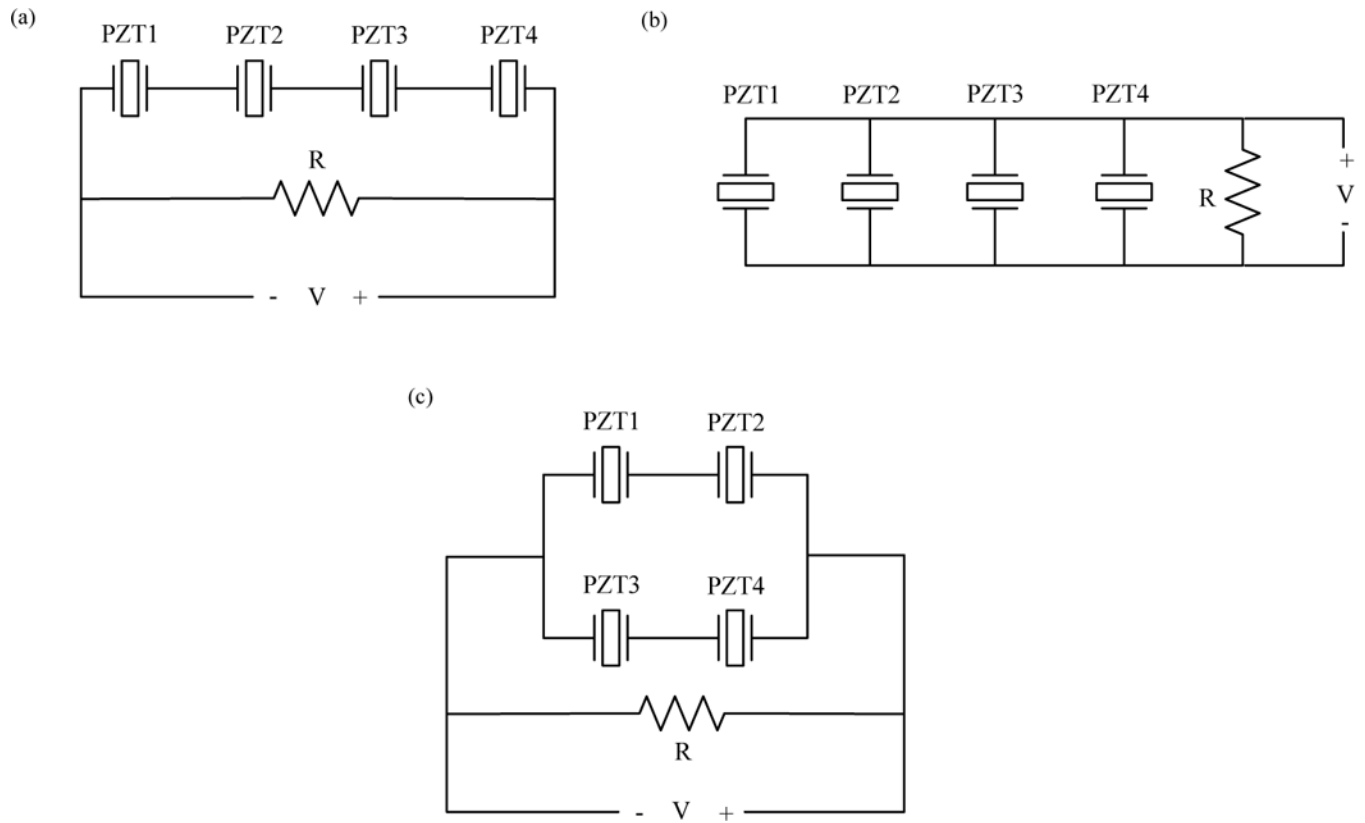


**Figure 6.** Experimental compression testing setup including (a) overall setup and (b) close-up view of the instrumented bearing and femoral component installed in the load frame.

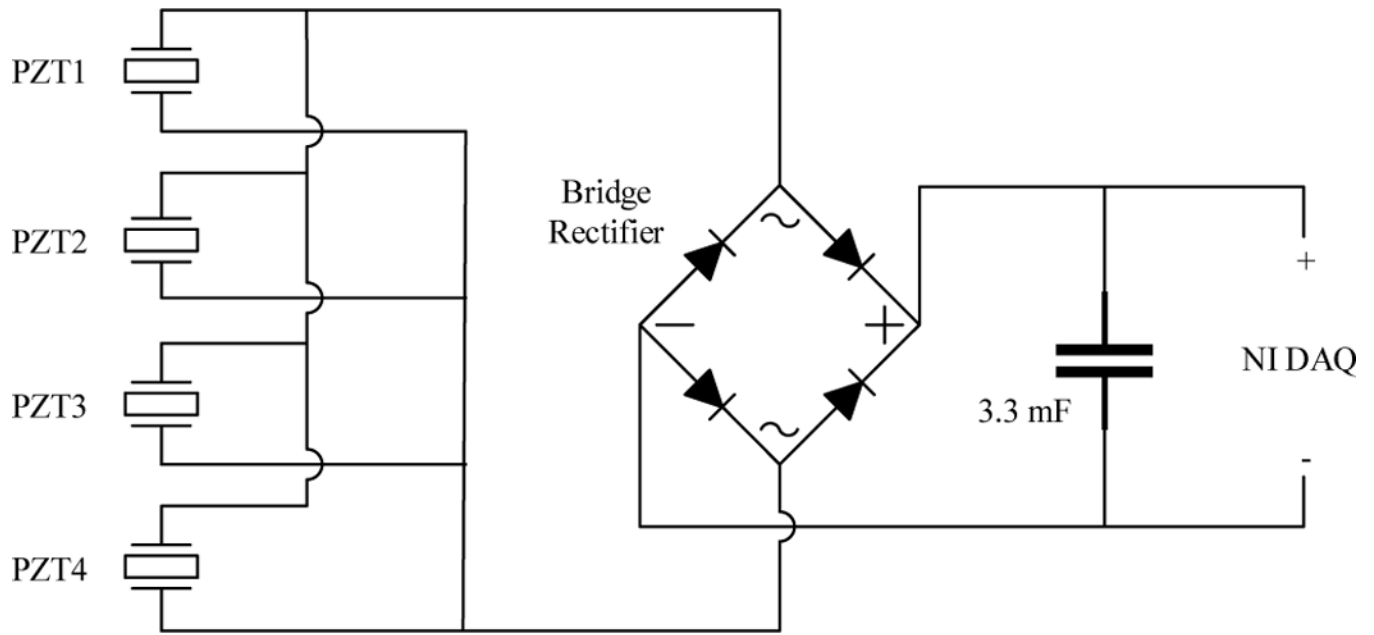


**Figure 7.**  
Schematic diagram of sensing circuit.

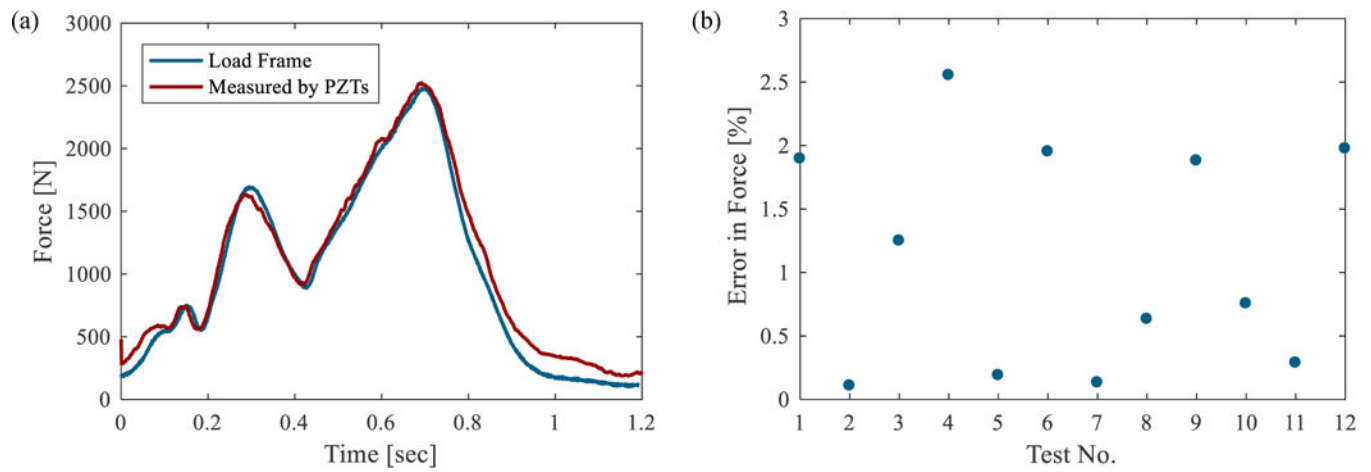




**Figure 8.** Schematic diagram of considered wiring configurations where PZTs are placed in (a) series, (b) parallel, and (c) combination of series and parallel .

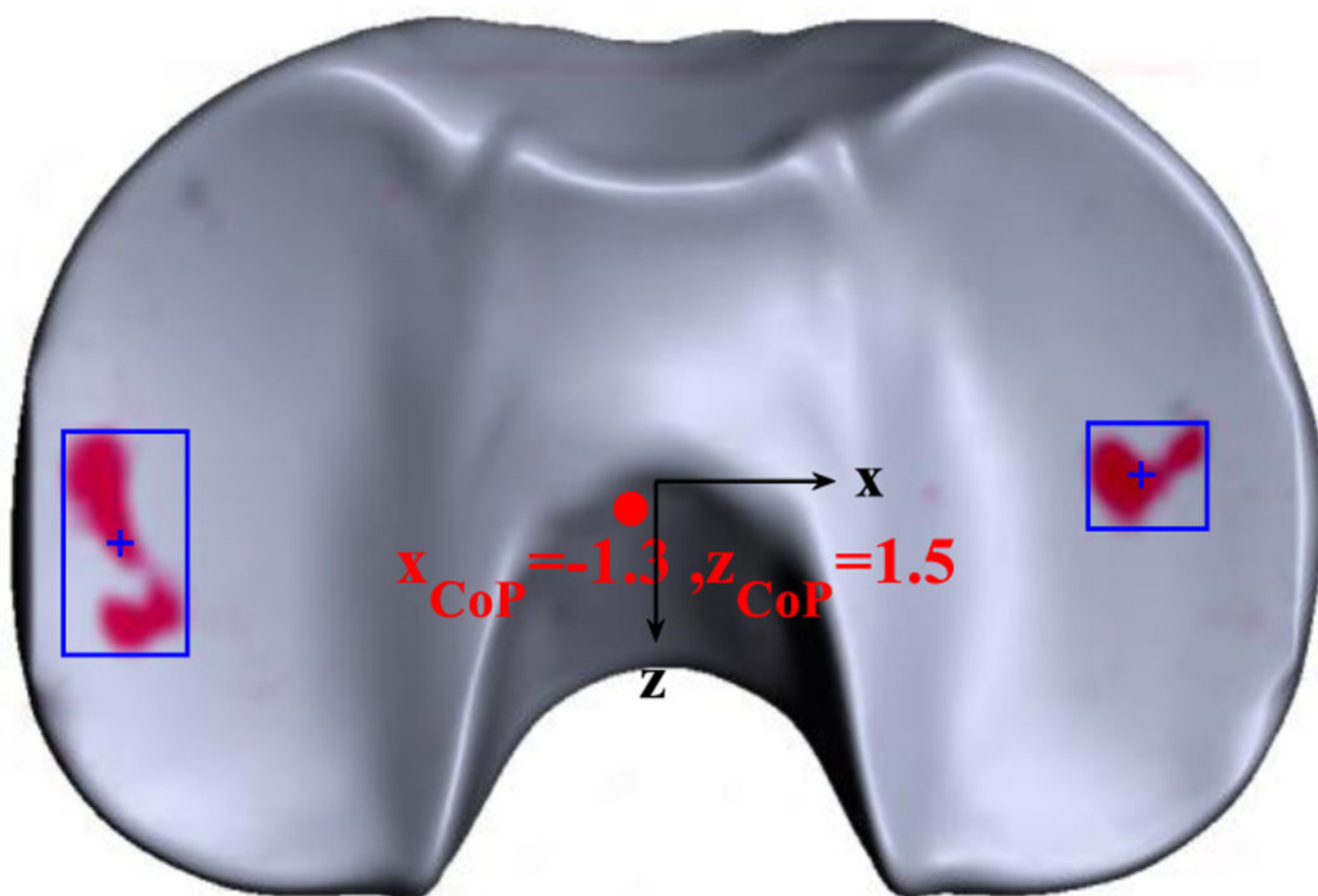


**Figure 9.**  
Schematic diagram of energy harvesting circuit including rectifier and power storage.



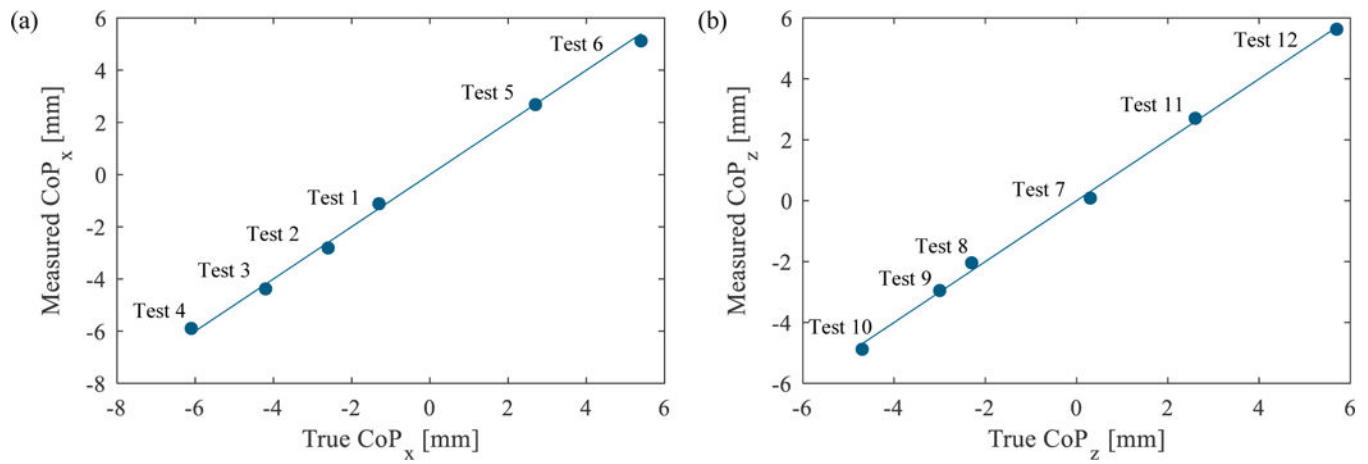
**Figure 10.**

(a) Comparison of measured and true total applied force profile for test 1, and (b) error in measured total force for 12 experiments.



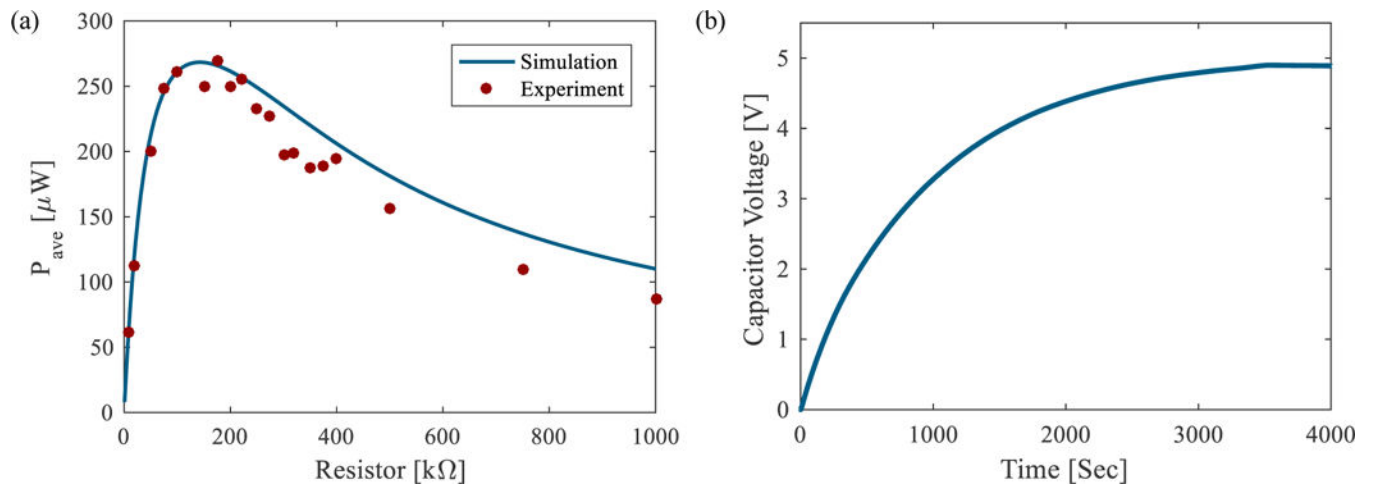
**Figure 11.**

Measured contact areas (red areas), centers of contact areas (blue plus signs), and CoP (red dot) from pressure sensitive film for Test 1 (all dimensions are in mm).



**Figure 12.**

Comparison of measured locations of CoP by PZTs and true locations from pressure sensitive films for (a) Tests 1–6 when the bearing is moved in x-direction, and (b) Tests 7–12 when the bearing is moved in z-direction.



**Figure 13.** Energy harvesting results showing (a) average power vs. resistive load, and (b) voltage on 3.3 mF storage capacitor vs. time.

**Table 1.**

Material properties for PLA and piezoelectric materials.

Material Properties	PLA Bearing [23]	NCE51 (PZT-5A) Piezoelectric [24]
Young's modulus [GPa]	3.5	52
Poisson's Ratio	0.42	0.35
Density [kg/m <sup>3</sup> ]	1240	7850
Piezoelectric Constant, $d_{33}$ [pC/N]	—	$443 \times 10^{-12}$
Piezoelectric Constant, $d_{31}$ [pC/N]	—	$-180 \times 10^{-12}$
Piezoelectric Constant, $d_{15}$ [pC/N]	—	$590 \times 10^{-12}$
Relative Permittivity, $\epsilon_{33}^T/\epsilon_0$	—	1900



**Table 2.**

Simulation parameters and results.

Simulation No.	Angle $\alpha_1$	Angle $\alpha_2$	Error in Total Force	Deviation in x (mm)	Deviation in z (mm)	Total Deviation (mm)
1	130.00	90.00	0.00%	0.26	0.19	0.32
2	90.00	90.00	0.00%	0.86	0.44	0.97
3	70.00	90.00	0.00%	0.89	0.65	1.10
4	50.00	90.00	0.00%	1.06	1.01	1.46
5	130.00	50.00	0.00%	0.67	0.79	1.04
6	90.00	50.00	0.00%	0.85	1.23	1.49
7	70.00	50.00	0.00%	1.34	0.15	1.35
8	50.00	50.00	0.00%	1.39	0.01	1.39
9	130.00	130.00	0.00%	0.76	0.08	0.76
10	90.00	130.00	0.00%	0.85	0.91	1.25
11	70.00	130.00	0.00%	1.10	2.10	2.37
12	50.00	130.00	0.00%	1.09	2.90	3.10

**Table 3.**

The relative location of femoral component and bearing for the sensing tests.

Test No.	Relative location in mm		Test No.	Relative location in mm	
	x-direction	z-direction		x-direction	z-direction
Test 1	0	0	Test 7	0	0
Test 2	-1.5	0	Test 8	0	-1.5
Test 3	-3	0	Test 9	0	-3
Test 4	-4.5	0	Test 10	0	-4.5
Test 5	+1.5	0	Test 11	0	+1.5
Test 6	+3	0	Test 12	0	+3

**Table 4.**

Characteristics of electrical circuits for various wiring configurations of PZTs.

Configuration	Governing Equation	Optimum Resistor		Maximum Power		Peak Voltage	
		Harmonic	Opensim	Harmonic	OpenSim	Harmonic	OpenSim
Single PZT	$C_p \frac{dV(t)}{dt} + \frac{V(t)}{R} = d_{33} \frac{dF(t)}{dt}$	$R_{opt}$	600 $k\Omega$	$P$	0.067 $mW$	$V_p$	6 $V$
PZTs in series	$C_p \frac{dV(t)}{dt} + \frac{4V(t)}{R} = d_{33} \frac{dF(t)}{dt}$	$4R_{opt}$	2400 $k\Omega$	$4P$	0.268 $mW$	$4V_p$	24 $V$
PZTs in parallel	$4C_p \frac{dV(t)}{dt} + \frac{V(t)}{R} = d_{33} \frac{dF(t)}{dt}$	$\frac{R_{opt}}{4}$	150 $k\Omega$	$4P$	0.268 $mW$	$V_p$	6 $V$
Combination of series and Parallel PZTs	$2C_p \frac{dV(t)}{dt} + \frac{2V(t)}{R} = d_{33} \frac{dF(t)}{dt}$	$R_{opt}$	600 $k\Omega$	$4P$	0.268 $mW$	$2V_p$	12 $V$